1) Explicit diffusion Option CISBA=DIF

A) Thermal Transfer and the surface Energy Budget (NP89 or PL98 thermal conductivity, DEF or MLCH surface heat capacity)

B) Hydrological Transfer (DEF or option KXP: expo. Ksat, WDRAIN 2D variable input)

2) Cold Season Processes CSNOW

A) Soil Phase changes

i) Phase changes based on water content (DEF)

ii) Phase changes based on water content and temperature (LWT)

B) Snowpack

- i) Single-layer bulk snow (EBA)
- ii) Composite snow (DEF)
- iii) Explicit Snow (3-L)

- DEF or RIL Rich. Number limit

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Options



Explicit soil DIFfusion Option: Downgradient thermal transfer and Richard's Eq.



Comparison: 2 force restore soil options verses DIFusion grid



Explicit soil DIFfusion Option: Downgradient thermal transfer and Richard's Eq.

3 Prognostic equations: N-layers for temperature, liquid water and soil ice:

$$c_{h}\frac{\partial T_{g}}{\partial t} = \frac{\partial G}{\partial z} + \Phi_{g}$$

$$\frac{\partial w_{l}}{\partial t} = -\frac{\partial F}{\partial z} - \frac{\Phi_{g}}{L_{f}\rho_{w}} - \frac{S_{l}}{\rho_{w}} \qquad (w_{min} \leq w_{l} \leq w_{sat} - w_{i})$$

$$\frac{\partial w_{i}}{\partial t} = \frac{\Phi_{g}}{L_{f}\rho_{w}} - \frac{S_{i}}{\rho_{w}} \qquad (0 \leq w_{i} \leq w_{sat} - w_{min})$$

 $w = w_l + w_i$ Total soil water





Vertical heat transfer:

- Simple down-gradient thermal transfer
- heat capacity and thermal conductivity based on texture, soil moisture (and possibly mulch in uppermost layer)

$$G = \lambda \frac{\partial T}{\partial z}$$
 Flux

$$c_{gj} = (1 - w_{sat})C_{soil}\rho_{soil} + w_{lj}c_w + w_{ij}c_i$$
 Heat capacity





Soil Thermal conductivity: CSCOND NP89: based on McCumber and Pielke (used implicitly in FR option) - no explicit accounting for soil ice

PL98: Peters-Lidard: shown to be more accurate for dry and wet soils, and includes soil ice.

- lower thermal wave penetration for wetter soils







The prognostic temperature equation for each layer also includes a phase change term (described later):

$$\Delta z_j c_{hj} \frac{\partial T_{g,j}}{\partial t} = G_{j-1} - G_j + \Delta z_j \Phi_{gj}$$

The Heat capacity is:
$$c_{h\,j} = \begin{cases} c_{g\,j} & (j=2,N) \\ 1/(C_T \Delta z_1) & (j=1) \end{cases}$$

So for the uppermost thin layer (surface energy budget):

$$\frac{1}{C_T} \frac{\partial T_s}{\partial t} = \frac{R_n - H - LE - G_1 + \Delta z_1 \Phi_{g,1}}{\text{Upper BC}}$$

$$C\tau \text{ takes into account soil and vegetation}$$
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The heat flux between the surface layer and the underlying soil is simply:

$$G_1 = 2\,\overline{\lambda}_1 \frac{(T_s - T_{g,2})}{\Delta z_1 + \Delta z_2}$$

$$\overline{\lambda}_1 = \frac{\Delta z_1 + \Delta z_2}{(\Delta z_1 / \lambda_s) + (\Delta z_2 / \lambda_2)}$$

Interfacial (AVG) thermal conductivity

$$\lambda_s = \left[1 - veg\left(1 - f_v\right)\right]\lambda_1$$

The surface thermal conductivity is reduced when *veg* is large: assumed to result owing to a mulch/organic layer. Option CDIFSFCOND = MLCH

- Has an insulating effect (decoupling of sfc-deep layers)





Vertical soil water transfer:

- Flux includes Darcy's Law, vapor diffusion (dry soils), and a linear drainage term (WDRAIN option). This is "mixed form" Richard's flux (using matric potential gradient)

$$F = -k \frac{\partial}{\partial z} \left(\psi + z \right) - \frac{D_{\nu\psi}}{\rho_w} \frac{\partial \psi}{\partial z} - K_d$$

$$F = -\eta \, \frac{\partial \psi}{\partial z} - \zeta$$

With no linear drainage and moist unfrozen soils, the above collapses into usual Darcy's law:

$$F = -k \frac{\partial}{\partial z} \left(\psi + z \right)$$





The linear drainage Is usually OFF, but can be turned on by giving a non-zero value for *Wdrain*...can maintain a nearly constant flow (to rivers...) even for fairly dry conditions.

$$K_{d} = k_{sat} [(w_{fc} + w_{drain}) / w_{sat}]^{2b+3} \times \left\{ \frac{[\min(w_{fc}, w_{l}) - w_{min}]}{(w_{fc} - w_{min})} \right\}$$

$$F_N = -\zeta_N = -k_N - K_d$$

 $I = -F_0 = \min(R_t - Q_r, -F_{max 0})$

 $F_{max0} = k_{sat}$

Water Flow Boundary Conditions:

Infiltration is the lesser of a maximum infitration rate and throughfall less subgrid surface runoff... Lower BC is free drainage.





Mixed-Form Richard's equation permits the use of heterogeneous soil texture profiles (since *psi* is continuous while water content is NOT under such conditions)

Vertical interpolation is based on the upper layer value in the presence of a wetting front, and relaxation to hydrostatic equilibrium otherwise (Noilhan and Planton, Koster and Suarez...etc...)







Example of heterogeneous Profile Application:

Soil texture profile at MUREX: (thick lines represent vertical averages)

- Result is significant gradient of hydrological parameters...







Using DIF with 7 layers (corresponding to each horizon plus thin upper layers for numerical reasons)

- Equilibrium soil water profiles using homogeneous and heterogeneous texture profiles







Heterogeneous Profiles better agree with observed soil moisture profile.

No options to specify: just prescribe sand and clay fractions by layer in NAMELIST







AMMA (ALMIP) Aug. 2006 : ISBA-DIF – volumetric water content



Hydrological Effect of soil ice:

Ice is assumed to become part of the solid soil matrix....

$$\Theta = \frac{w - w_i}{w_{sat} - w_i} = \frac{w_l}{w_{sat\,l}} \qquad (0 \le \Theta \le 1)$$

$$k = k_{sat} \Theta^{2b+3}$$

$$\psi = \psi_{sat} \Theta^{-b}$$

 $\wp = 10^{-a_{\wp} w_i/w}$

When a layer freezes, this can create strong liquid water gradients, so a diffusion impedance term is used







Reduction factor for vertical soil water diffusion for different values of parameter *Eice* as a function of ice fraction in the soil.



Phase Changes in the Soil: CSOILFRZ=DEF option

The freeze/thaw rates are proportional to the temperature depression and the available liquid/ice.

$$\Phi_{fj} = \min \left[K_s \epsilon_f \max \left(0, T_f - T_j \right) c_i, \\ L_f \rho_w \max \left(0, w_{lj} - w_{\min} \right) \right] / \tau_i$$

$$\Phi_{mj} = \min \left[K_s \epsilon_m \max \left(0, T_j - T_f \right) c_i, \ L_f \rho_w w_{ij} \right] / \tau_i$$

$$\epsilon_j = \begin{cases} w_{lj} / (w_{sat} - w_{ij}) & (T_j \leq T_f) \\ \\ w_{ij} / (w_{sat} - w_{min}) & (T_j > T_f) \end{cases}$$
$$K_s = \left(1 - \frac{veg}{K_2}\right) \left(1 - \frac{LAI}{K_3}\right) & (0 < K_s \leq 1) \end{cases}$$

Rate of freeze thaw a function of efficiency and vegetation (Bazile)

ours un temps d'avance



Example setup for Illinois:

Test soil freezing impact on soil temperatures, surface fluxes...

Examine 2 cold periods in 98-99











Impact of soil freezing on surface temperatures during 2 cold periods...night-time cold bias all but removed





Option CSOILFRZ=LWT: As opposed to potentially

freezing ALL liquid water, this method uses the freezing curve method. The maximum liquid water content for a given texture is a function of T...

More physical...

also avoids numerical problems since liquid water content stays above minimum numerical threshold







Snow scheme options: CSNOW

<u>EBA</u> - Bazile composite scheme, 2 prognostic variables NWP usage and improved fcst scores

<u>DEF</u> - Douville composite scheme, 3 prognostic variables Extensive use in offline and GCM

<u>3-L*</u> - Boone (ISBA-ES: Explicit Snow), 4 prognostic variables (3-N layer variables, 1 single layer var) Offline and Mesoscale modelling, operational Hydro

* **Ongoing developments:** new modifications with snow grain variables, history variables, 10 layers....coupling with vegetation canopy





DEF - Composite snow scheme EBA - Composite (**no** density prognostic eq)





- DEF Composite snow scheme
- EBA Composite (no density prognostic eq)

$$\frac{\partial W_n}{\partial t} = P_n - E_n - F_n$$

$$\frac{\partial \rho_n}{\partial t} = \frac{\tau_f}{\tau} \left(\rho_{\max} - \rho_n \right) \qquad \left(\rho_{\min} \le \rho_n \le \rho_{\max} \right)$$

$$\frac{\partial \alpha_n}{\partial t} = \frac{-1}{\tau} \left[\delta_\alpha \tau_f \left(\alpha_n - \alpha_{\min} \right) + \left(1 - \delta_\alpha \right) \tau_a \right] + \frac{P_n}{W_{crn}}$$

$$F_n = p_n \frac{(T_n - T_f)}{C_n L_f \Delta t} \qquad (F_n \ge 0)$$

$$T_n = (1 - veg)T_s + veg T_2$$

$$F_n = P_n \frac{(T_n - T_f)}{C_n L_f \Delta t}$$







Default **snow fraction** for baresoil (*png*) for all models, *pnv* used for 3-L and DEF (EBA based on *LAI* and *age* also, results in significantly improved T2m air temperatures over Northern Hemisphere)

soil
$$p_{ng} = W_n / (W_n + W_{crn})$$
 $(W_{crn} = 10 \text{ kg m}^2)$
veg $p_{nv} = h_n / (h_n + 5z_0)$
 $p_n = veg p_{nv} + (1 - veg) p_{ng}$, TOTAL snow cover fraction

* Loosely physically based...mostly empirical...but...rather standard! Future developments may include topographic index/exposition, improvements using satellite-based data...







3-L: ISBA-ES is more detailed:

- an N-layer scheme (default 3)
- explicit compaction (and melt densification)
- radiative transfer
- explicit energy budget: prognostic vars = albedo, density, SWE and H
- liquid water content (using enthalpy concept)

$$H_{s\,i} = c_{s\,i} \, D_{s\,i} \, \left(T_{s\,i} - T_f \right) \, - \, L_f \, \left(W_{s\,i} - W_{l\,i} \right) \qquad \begin{array}{l} {\rm New \ prog.} \\ {\rm variable} \end{array}$$

2 prognostic variables "for the price of one"...

$$T_{s\,i} = T_f + (H_{s\,i} + L_f W_{s\,i}) / (c_{s\,i} D_{s\,i}) \qquad (W_{l\,i} = 0)$$
$$W_{l\,i} = W_{s\,i} + (H_{s\,i}/L_f) \qquad (T_{s\,i} = T_f)$$





Time varying layer thicknesses

Total snowpack mass and energy conserved as grid changes in *t*





Grid and numerical setup essentially the same as for the soil heat diffusion Equation (DIF)















Example using **RIL**:

Impact of Using RIL option (with Richmax=0.20) at Col de Porte for 3 years. Good improvement...also impacts melting.



Phase changes and liquid water budget:

- relatively simple ("tipping bucket" hydrology)

- phase changes don't change *H*, but partitioning between *T* and *W*/ (unless runoff/mass loss)

$$F_{sm\,i} = \min \left[c_{s\,i} \, D_{s\,i} \, \left(T_{s\,i} - T_f \right), \ L_f \left(W_{s\,i} - W_{l\,i} \right) \right] / \Delta t$$

$$F_{sf\,i} = \min \left[c_{s\,i} \, D_{s\,i} \, \left(T_f - T_{s\,i} \right), \ L_f W_{l\,i} \right] / \Delta t \ .$$

$$F_{s\,i} = F_{sm\,i} - F_{sf\,i}$$

$$\frac{\partial W_{l\,i}}{\partial t} = R_{l\,i-1} - R_{l\,i} + F_{s\,i}/L_f \qquad (W_{l\,i} \le W_{l\,i\,\max})$$









Figure 5: Impact of the new scheme on the T_{2m} 96h forecast (avraged on the 15 runs).



From E. Bazile, GMAP





ISBA-ES

Off-line simulation for Col de Porte (1994-95)

Observed SWE, Depth

Using default 3L configuration





Profile – Simulations for Col de Porte

- Annual cycle
- by Eric Brun, using ISBA-ES with 10 layers (addtion by V. Vionnet)







<u>Contact:</u>

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Bertrand Decharme (soil, hydrology)

GAME-CNRM Météo-France

GAME-CNRM





extra.....





AVG Sim • AVG Obs





Compaction/settling in snow 3-L:

- function of temperature, density
- overlying weight of snow

Initialize with fresh snow density and 1m depth for 2 different constant T profiles...

