

**Improving the SURFEX/TEB scheme:
1-D validation in a street canyon**

R. Hamdi and V. Masson

**SURFEX coupled off-line to ALADIN:
preliminary results over Belgium**

R. Hamdi and A. Deckmyn

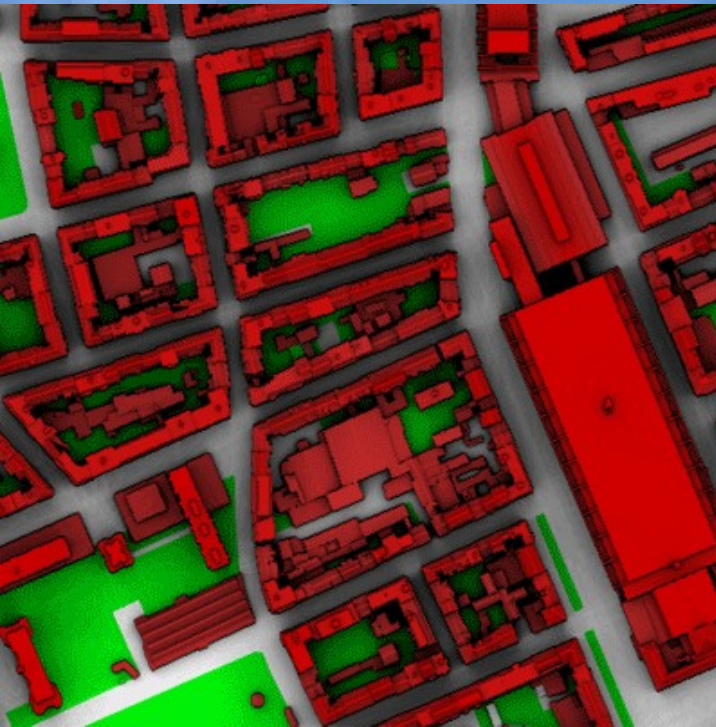
ALADIN-2007-Oslo (Norway) 23-26 April 2007

Improving the SURFEX/TEB scheme: 1-D validation in a street canyon

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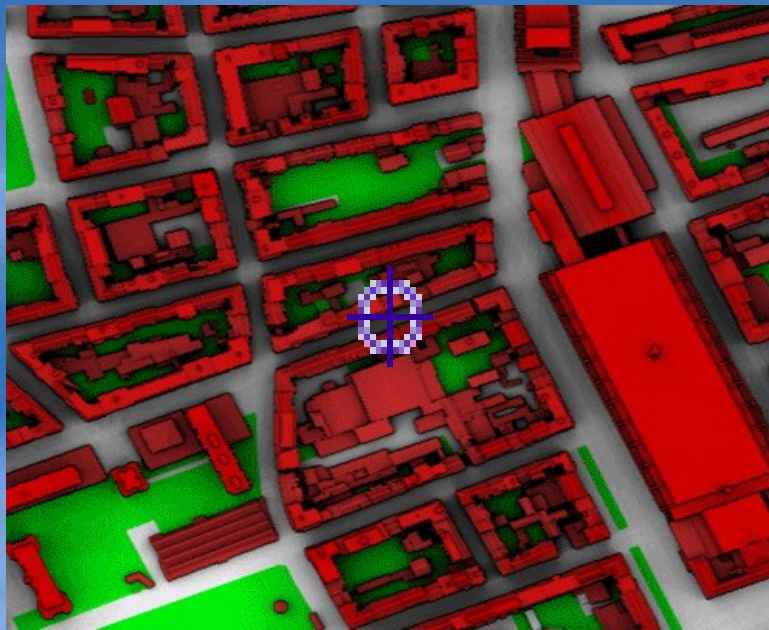
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Plan

- **Measurement site (BUBBLE)**
(**B**asel **U**r**B**an **B**oundary **L**ayer **E**xperiment)
- **The TEB scheme**
- **Improving the parameterization**
- **Results and discussions**
- **Conclusion**

Basel Sperrstrasse (U1)



Tower height : 32 m
Building height : 14.6 m
% Roof : 54%
% Vegetation : 16%
Wall/plane area ratio : 0.68
Canyon aspect ratio H/W : 1

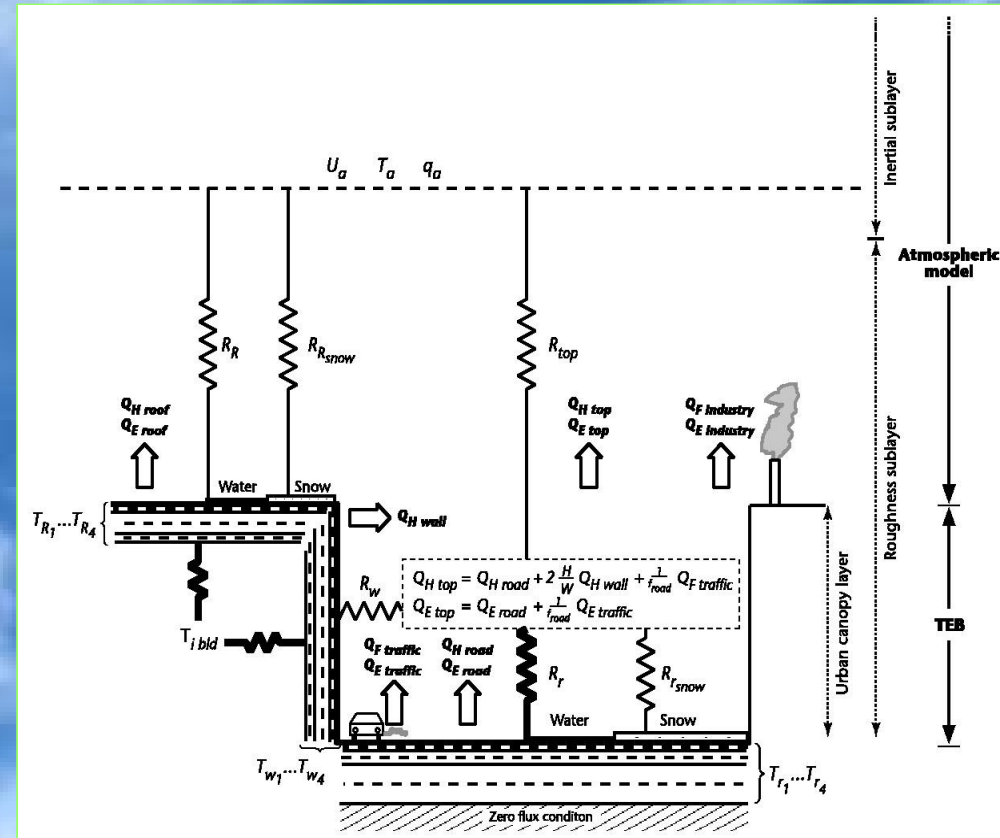
T, U, V, q, TKE, Q_H , Q_E \Rightarrow A, B, C, D, E, F (Ultrasonic anemometer-thermometer)

Q^* , $K\downarrow$, $K\uparrow$, $L\downarrow$, $L\uparrow$ \Rightarrow 3.2 m et 31.5 m (Pyranometer, Pyrgeometer)

Urban parameterization

TEB (Masson 2000)

- * Ensemble of urban canyons
- * Surface temperatures resolved for each of the 3 urban surfaces
roads, roofs and walls
- * Surface energy budget resolved for each urban surface
- * The averaged fluxes are calculated at the top of the canyon via the aerodynamic resistances
- * Diagnostic temperature and wind inside the canyon



Masson et al. 2002

Improving the parameterization (1)

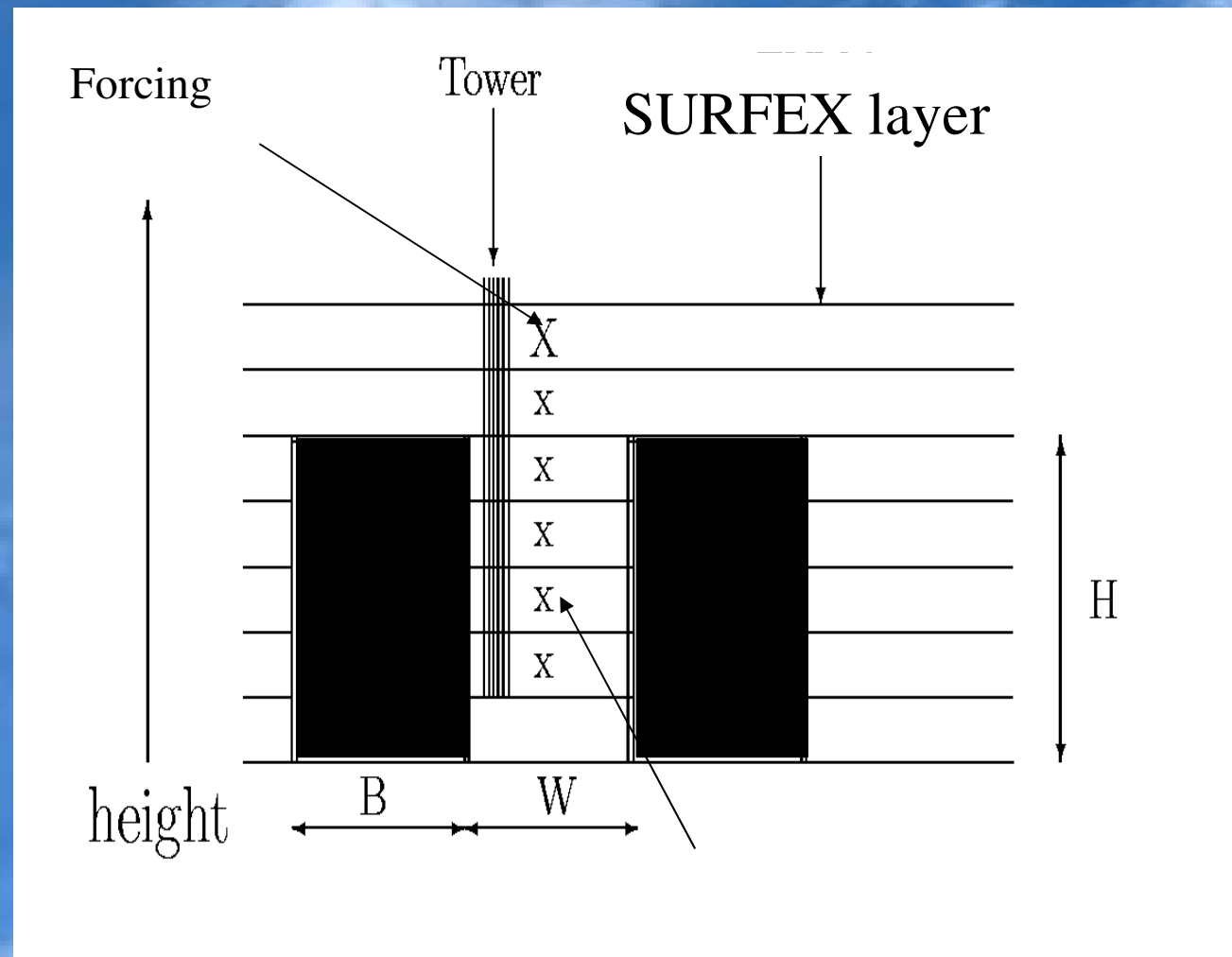
1. Surface scheme

$$\frac{\partial u}{\partial t} = \dots + \frac{\partial u}{\partial t} \Big|_{TEB}$$

$$\frac{\partial T}{\partial t} = \dots + \frac{\partial T}{\partial t} \Big|_{TEB}$$

$$\frac{\partial Tke}{\partial t} = \dots + \frac{\partial Tke}{\partial t} \Big|_{TEB}$$

$$\frac{\partial q}{\partial t} = \dots + \frac{\partial q}{\partial t} \Big|_{TEB}$$



Improving the parameterization (2)

1. Momentum

* Vertical surfaces (Walls):

$$\left. \frac{\partial U}{\partial t} \right|_{TEB} = -C_D (S_v / V_{air}) U^2$$

U wind speed, S_v ; S_h vertical (horizontal) surface area of the buildings, C_D drag coefficient.

* Horizontal surfaces (roads, roofs):

$$\left. \frac{\partial U}{\partial t} \right|_{TEB} = -U_*^2 (S_h / V_{air})$$

2. Turbulent kinetic energy

Production of turbulence by walls:

$$\left. \frac{\partial Tke}{\partial t} \right|_{TEB} = C_D (S_v / V_{air}) U^3$$

3. Temperature

* The heat turbulent fluxes Q_h are calculated between roof/road/wall and the atmosphere.

* This term is added at each atmospheric level in contact with the buildings.

$$\left. \frac{\partial T}{\partial t} \right|_{TEB} = \frac{(Q_h^{roof} + Q_h^{road})}{\rho C_p} (S_h / V_{air}) + \frac{Q_h^{wall}}{\rho C_p} (S_v / V_{air})$$

4. Mixing length

Modification of the mixing length L_m in the presence of buildings according to (Macdonald, 2000 ; Belcher et al. 2003):

$$L_m = H \quad \text{if} \quad z < H$$
$$L_m = H + \frac{z - H}{z(top) - H} [L_m(top) - H] \quad \text{if} \quad z \geq H$$

1-D SURFEX configuration

% ISBA = 16%

% TEB = 84%

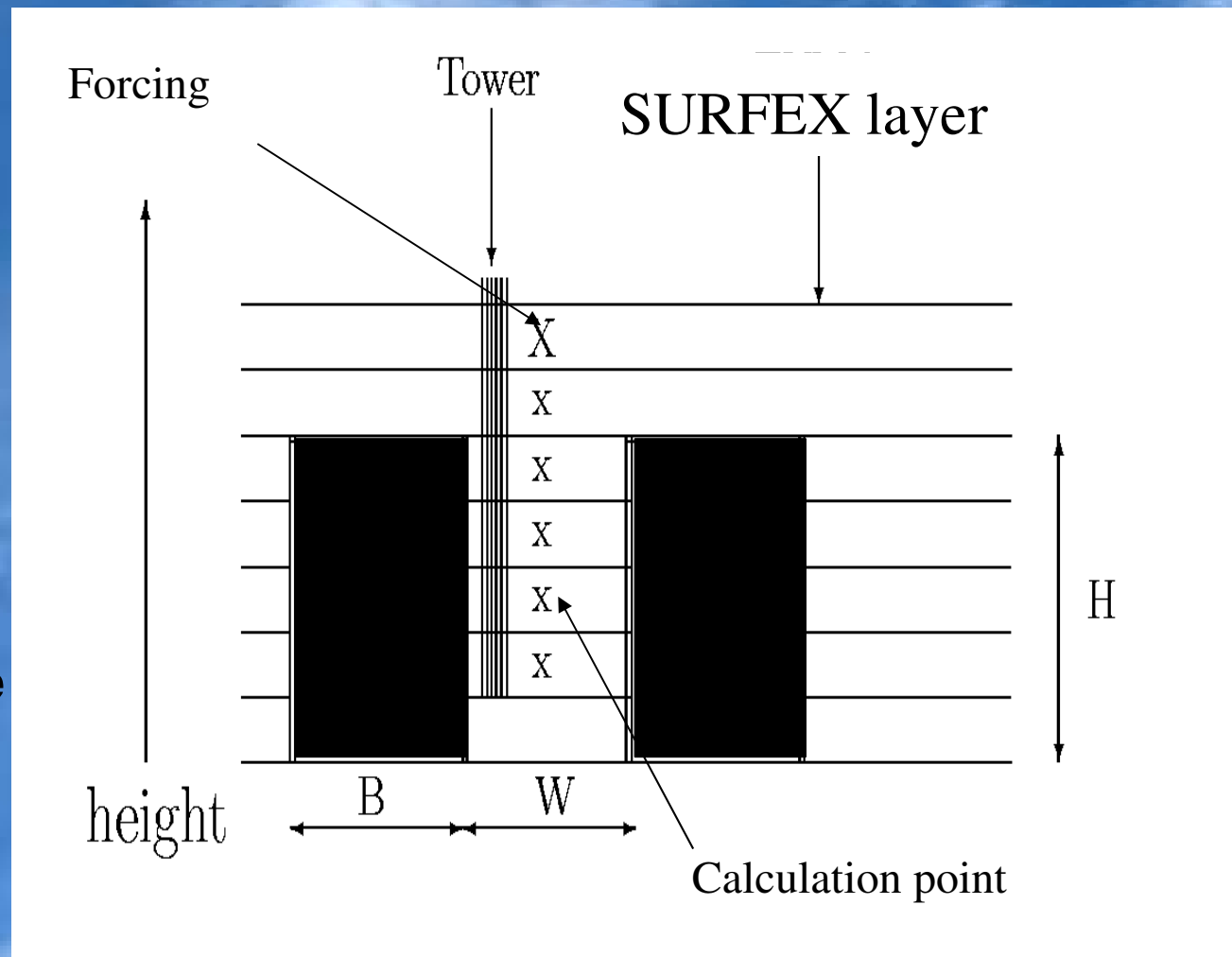
with % roof = 54%

The period of the simulations
from **16/06/2002** to **30/06/2002**

Forcing is applied with 10-min time
step to:

wind
Temperature
Humidity

downward global short- and long-
wave radiation.

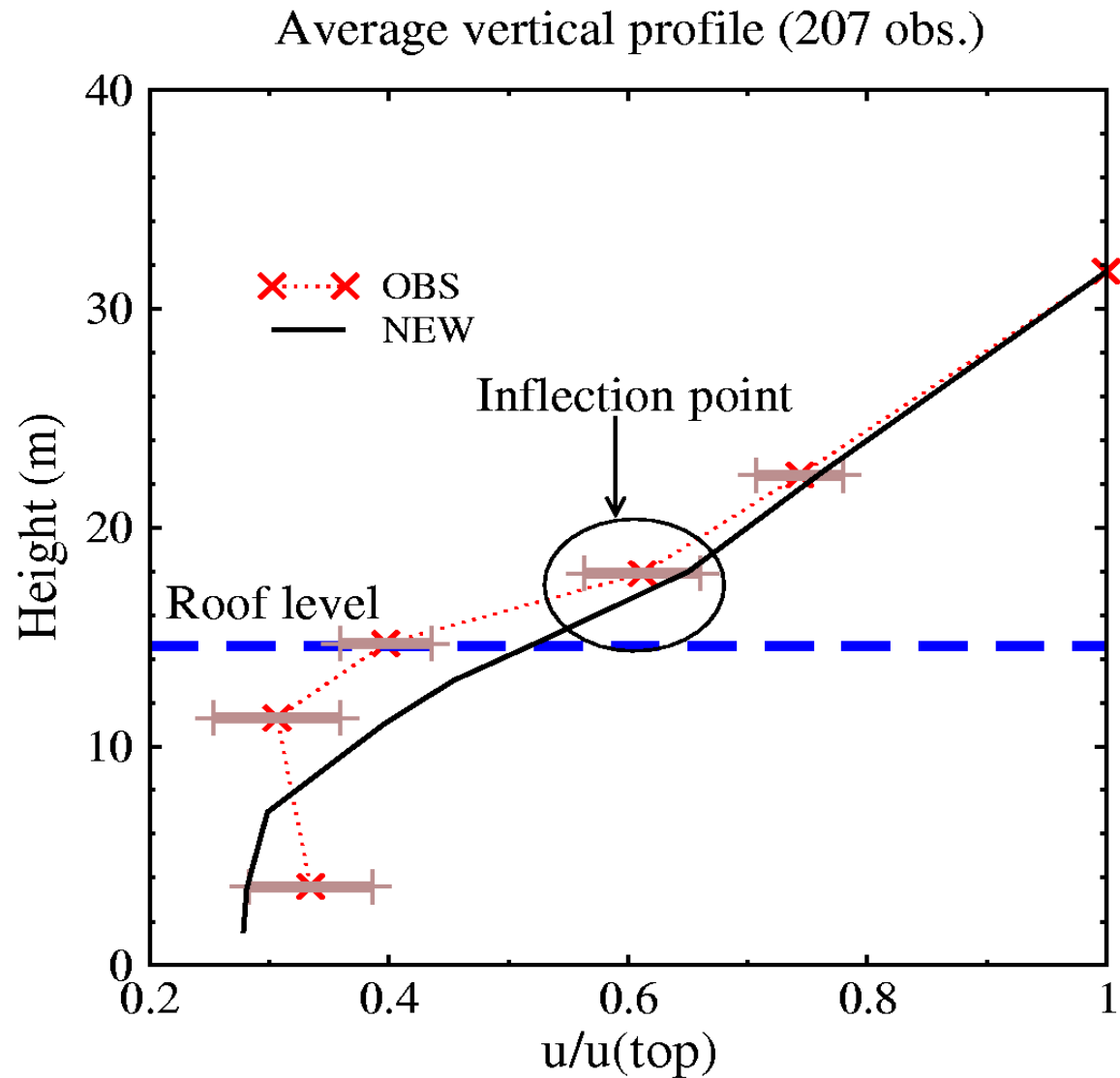


Two simulations:

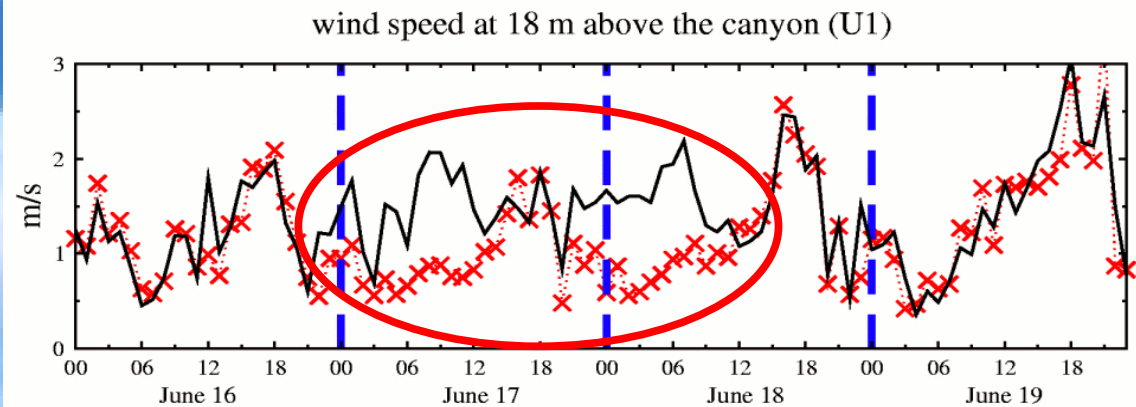
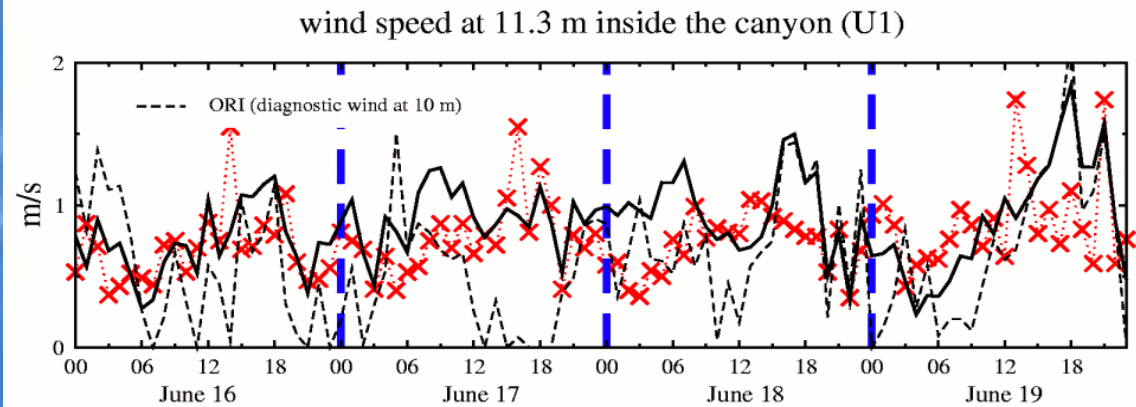
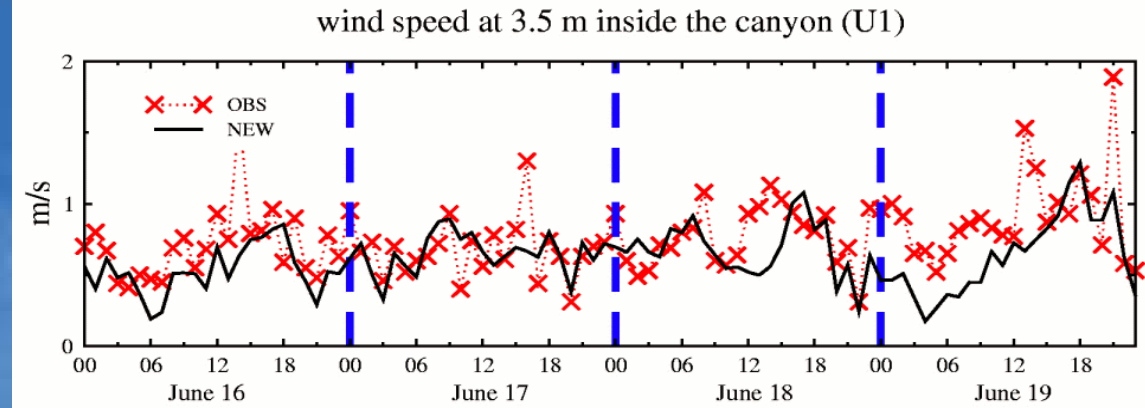
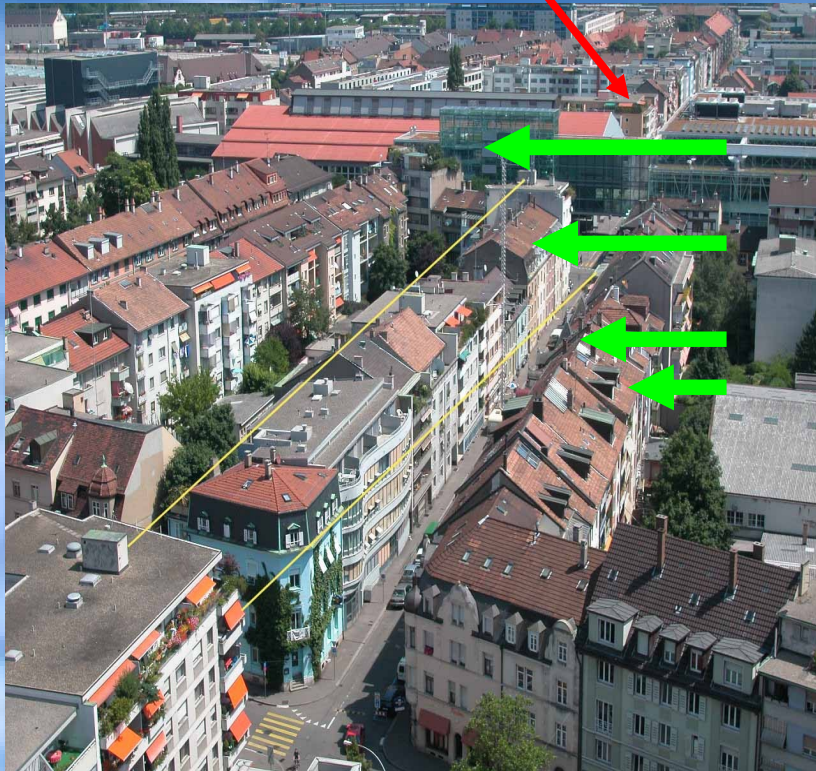
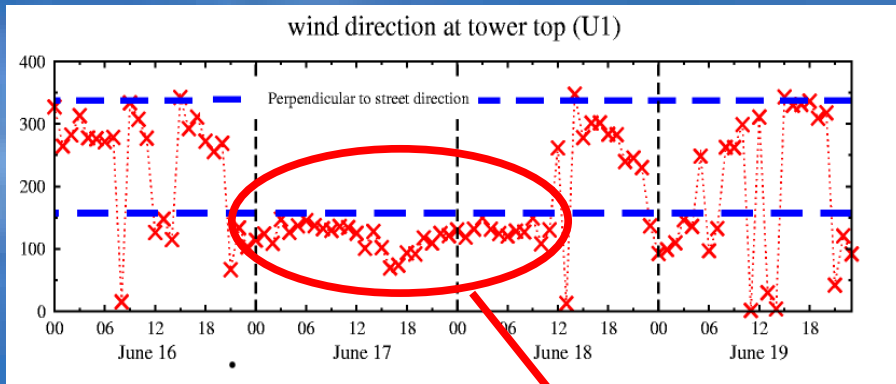
"NEW" with the prognostic version of SURFEX

"ORI" with the diagnostic version of SURFEX.

Results: wind speed

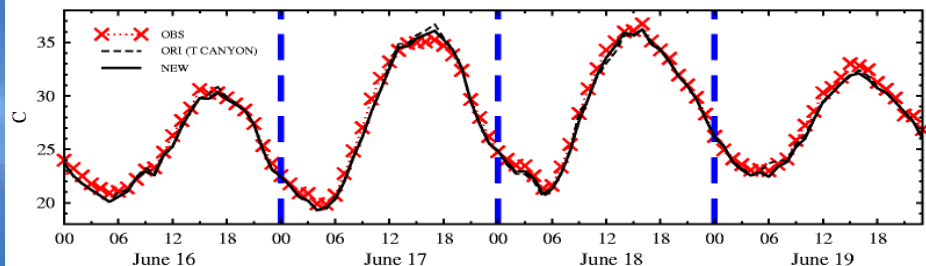


Results: wind speed

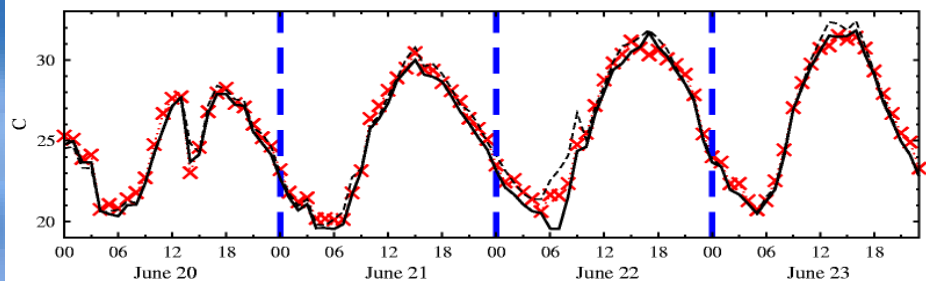


Results: temperature

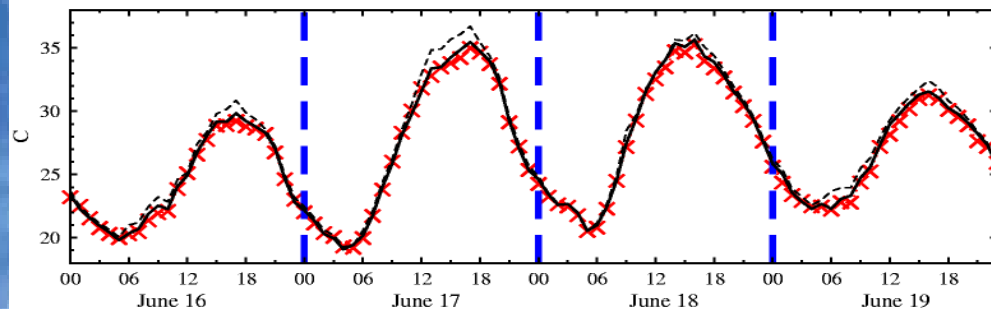
Temperature at 2.5 m inside the canyon (U1)



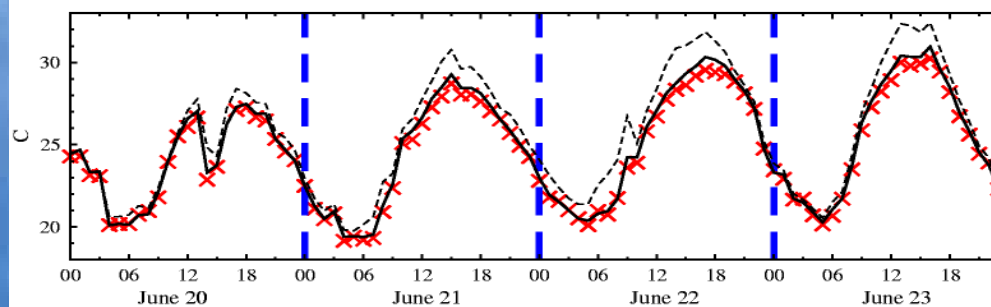
Temperature at 2.5 m inside the canyon (U1)



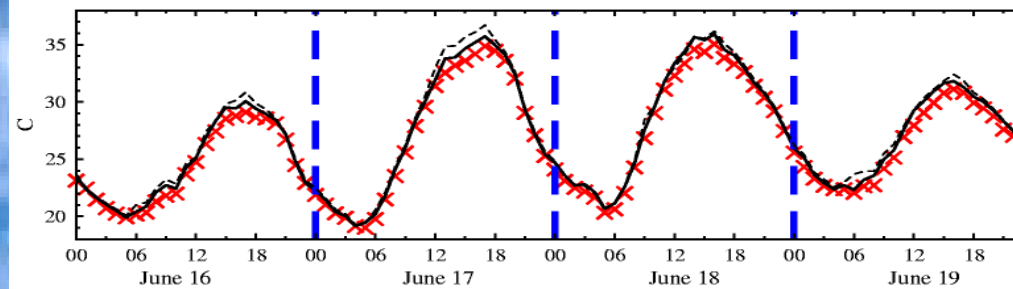
Temperature at 18 m above the canyon (U1)



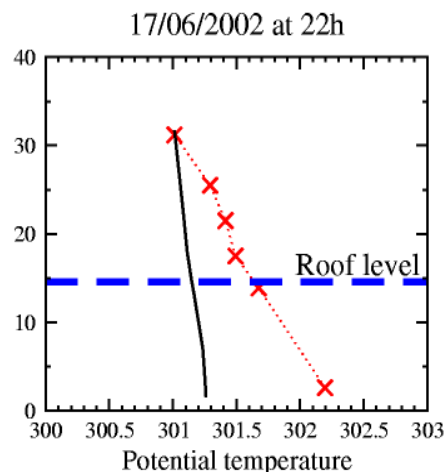
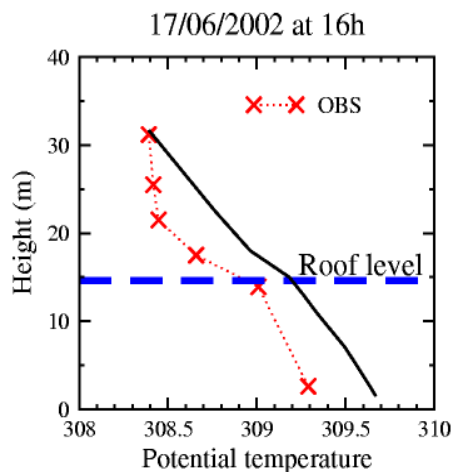
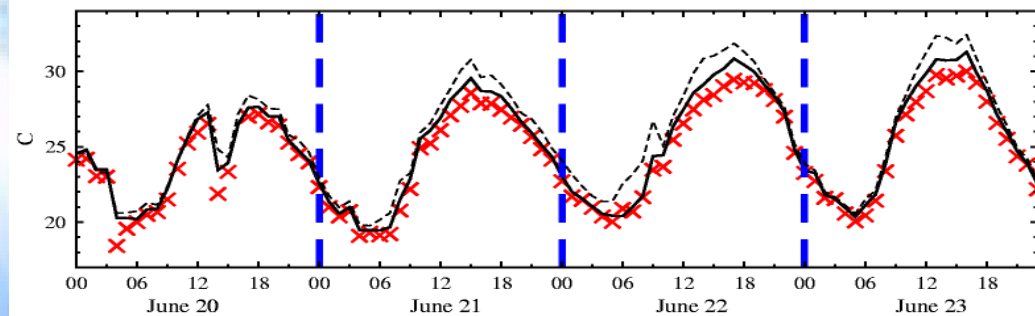
Temperature at 18 m above the canyon (U1)



Temperature at 14 m inside the canyon (U1)

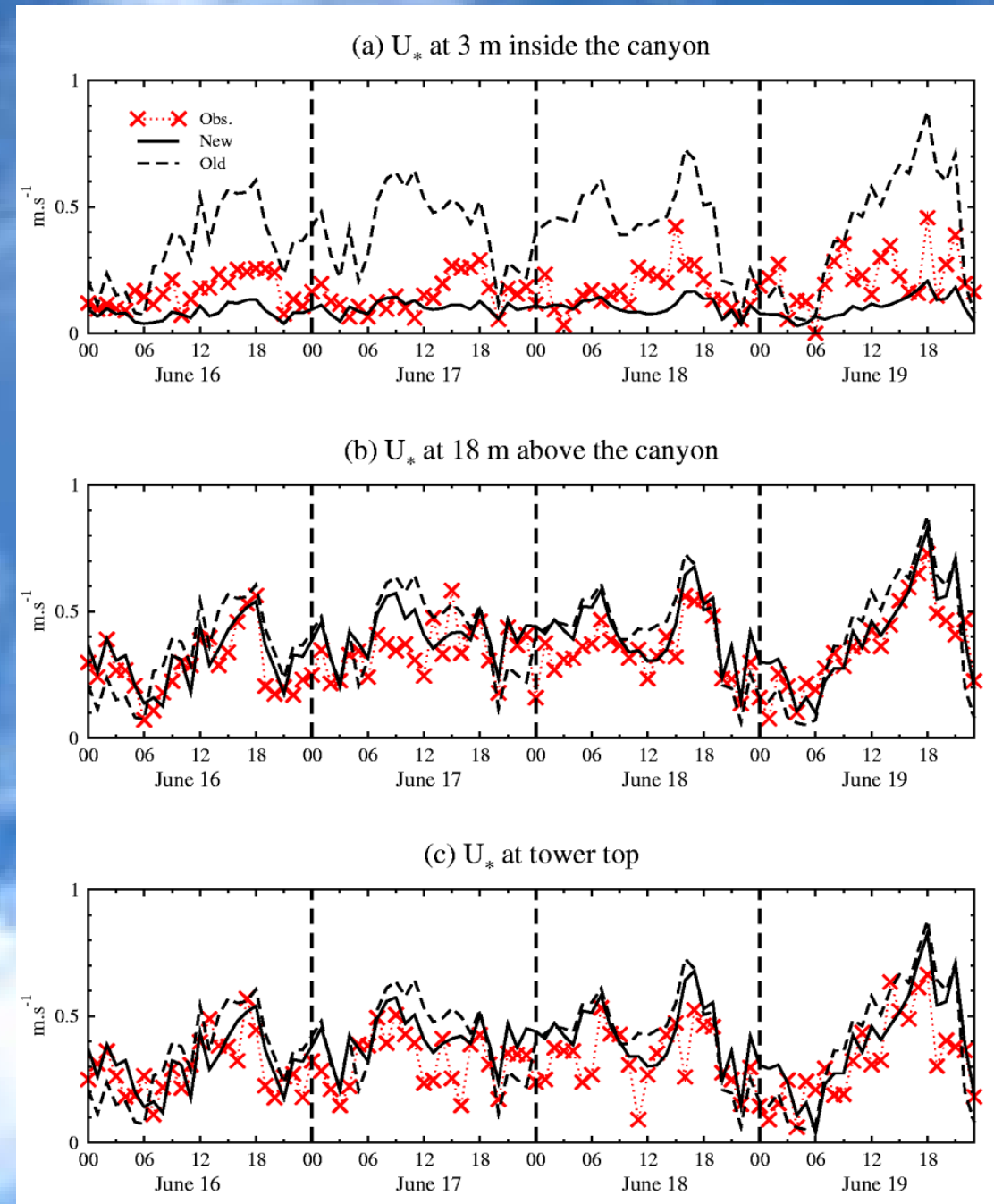
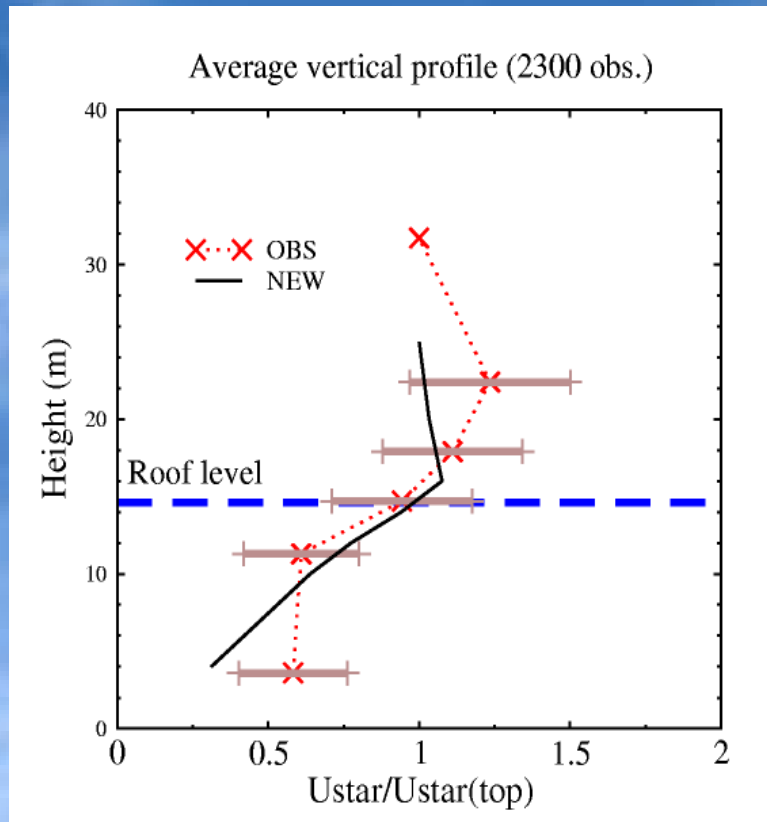


Temperature at 14 m inside the canyon (U1)

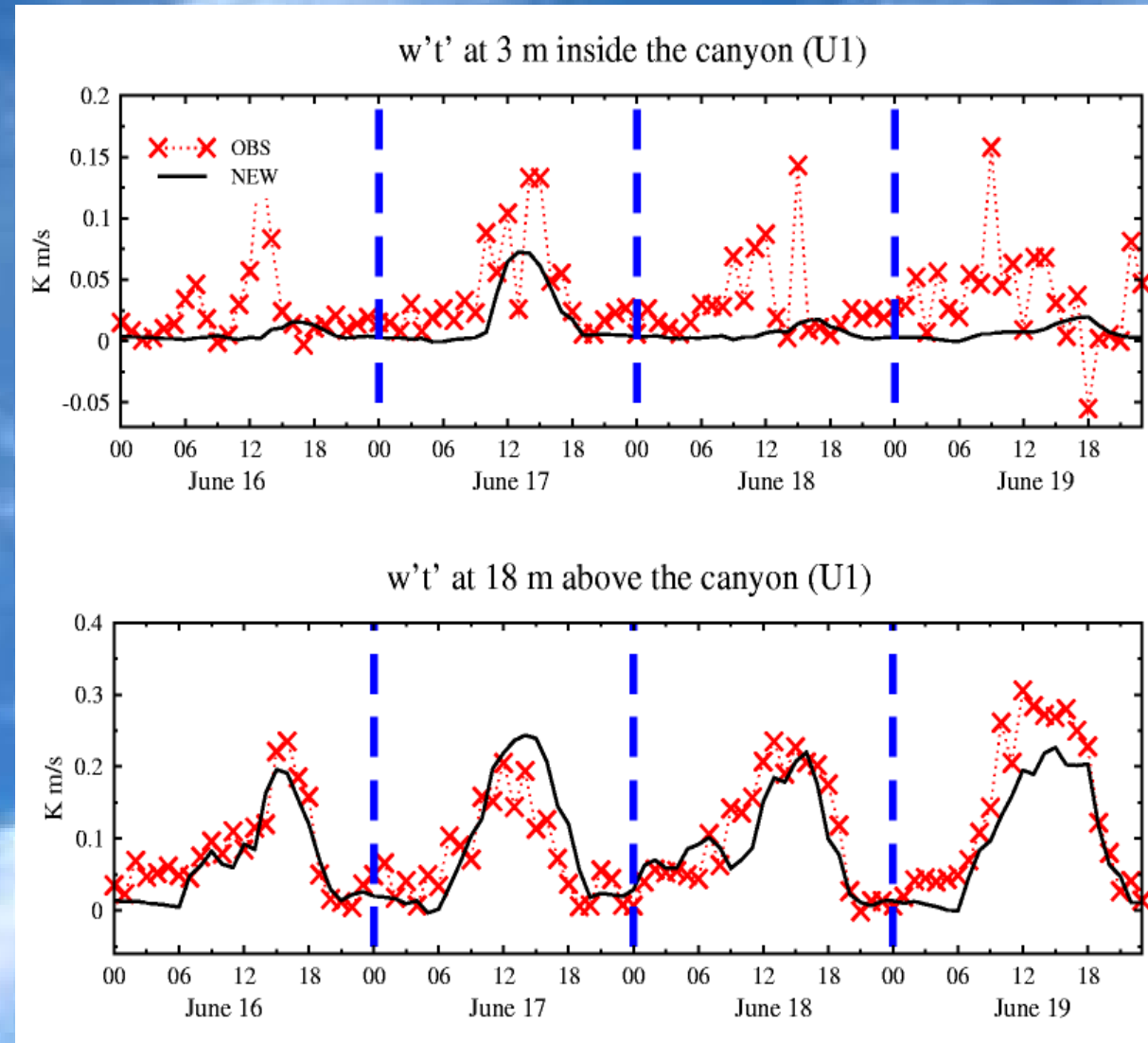
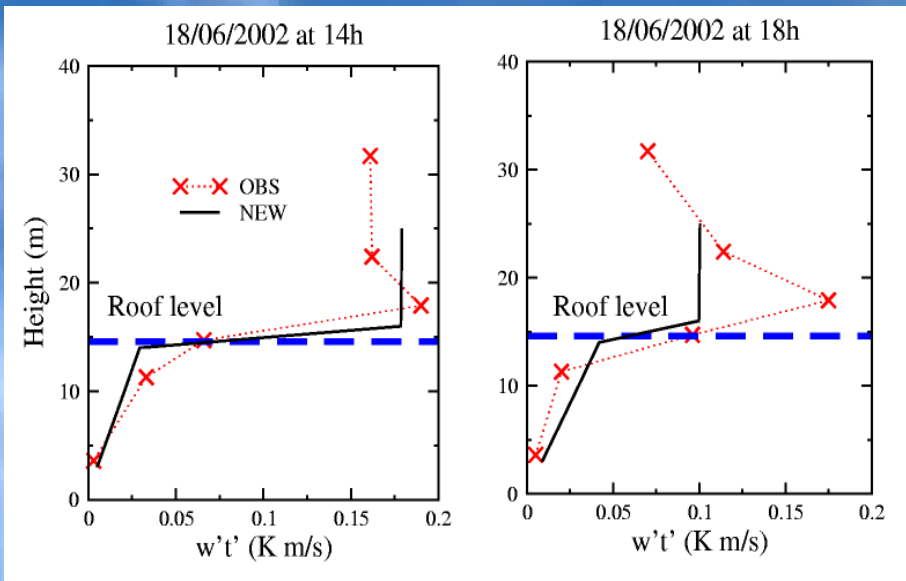


Results: momentum exchange

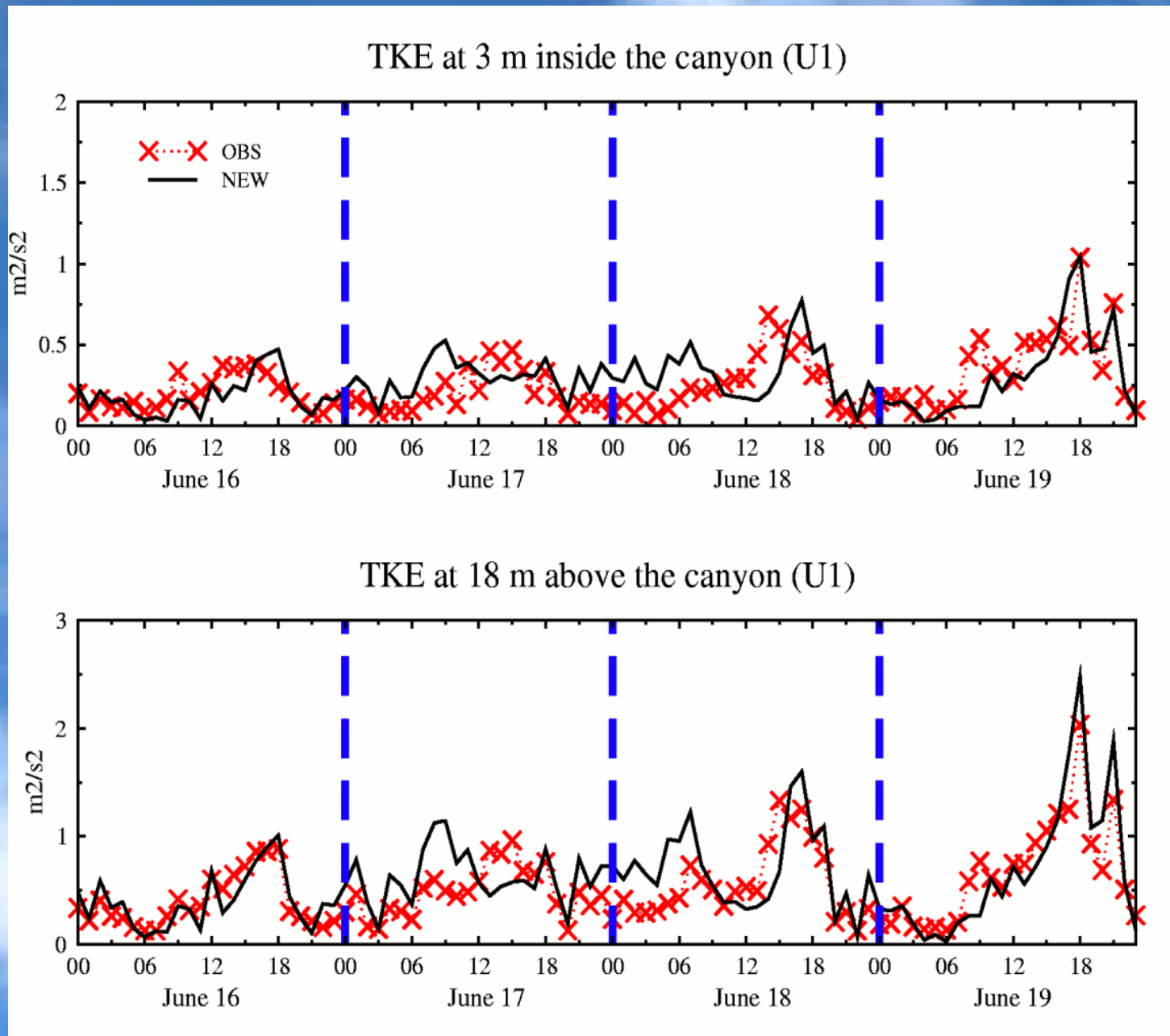
$$U_* = (\overline{w'u'^2} + \overline{w'v'^2})^{\frac{1}{4}}$$



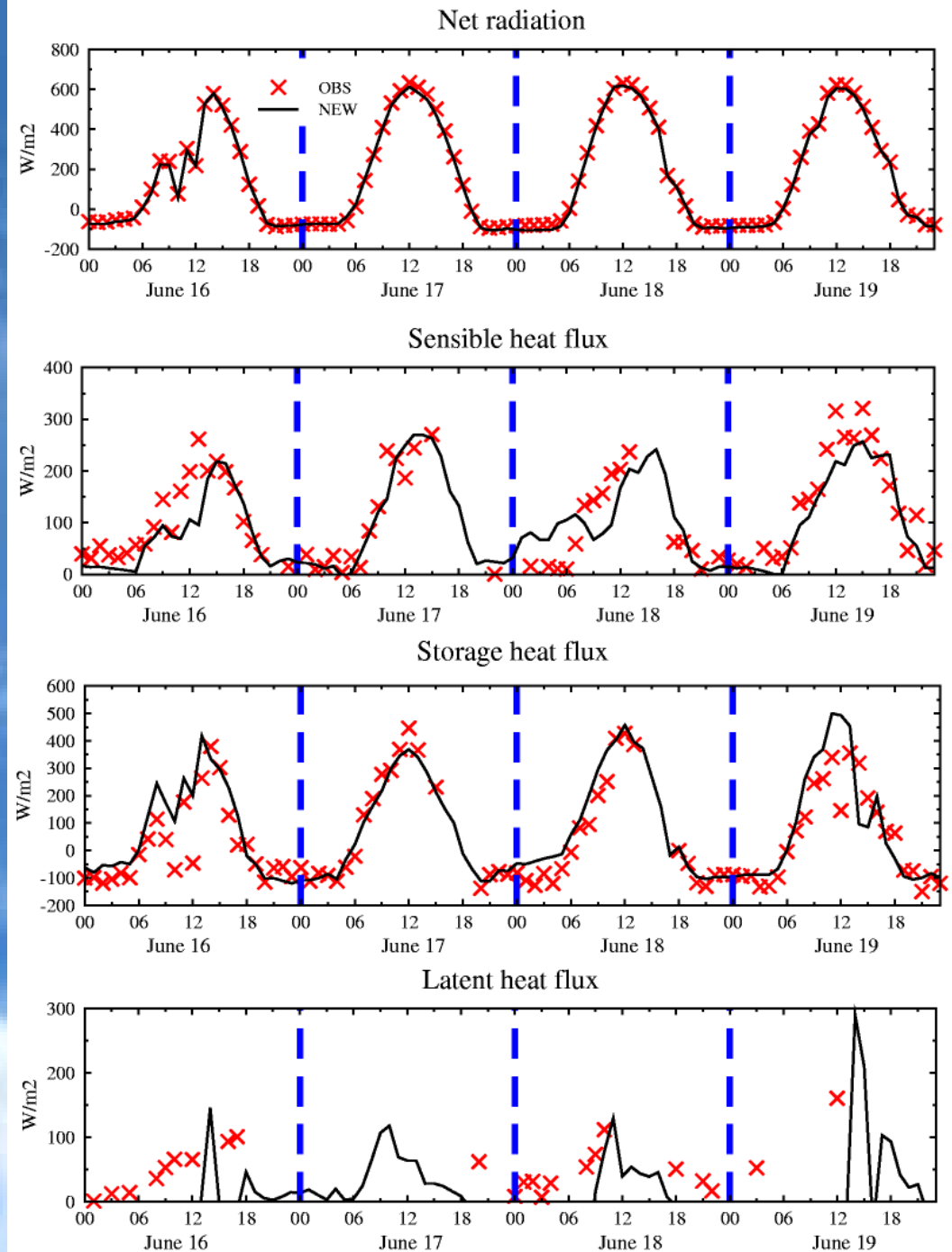
Results: turbulent exchange of heat



Results: turbulent kinetic energy



**Results:
energy balance at the
top of the canyon**



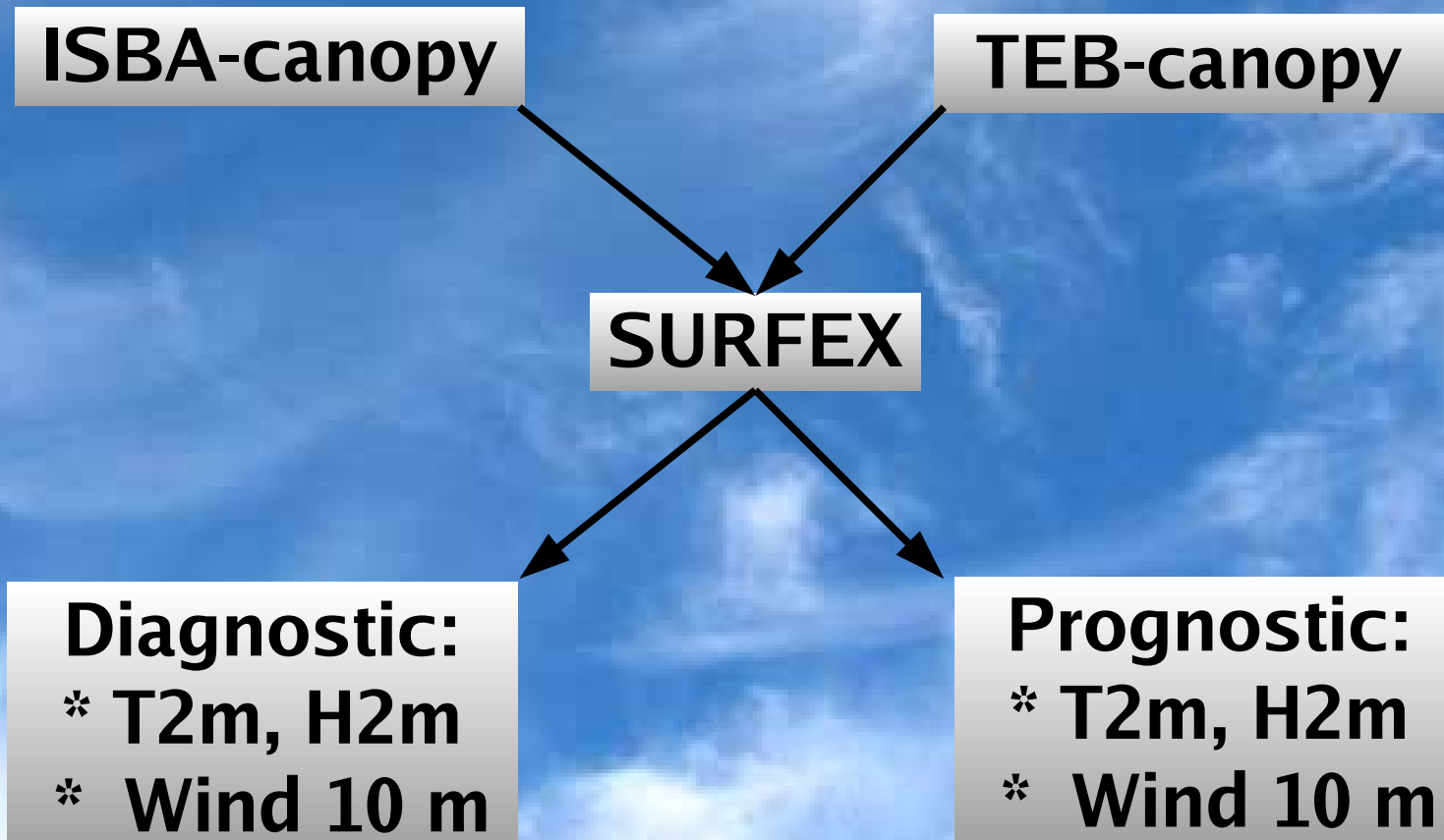
Conclusion

Bias = New(Ori)-Obs ; RMSE is the root-mean-square error.

	U(m.s ⁻¹)			T (°C)			U* (m.s ⁻¹)		Q _H (W.m ⁻²)	
Level (m)	3	11.3	18	2.5	14	18	3	18	31.5	31.7
Obs	0.83	0.80	1.31	27.14	26.01	26.18	0.16	0.33	0.33	86.18
New	0.63	0.87	1.42	26.73	26.52	26.35	0.10	0.39	0.39	78.00
Ori	---	0.74	---	26.70	26.70	---	0.39	0.39	0.39	122.8
Bias-New	-0.20	0.08	0.11	-0.40	0.50	0.17	-0.06	0.06	0.06	-8.00
Bias-Ori	---	-0.06	---	-0.43	0.68	---	0.23	0.06	0.06	36.60
RMSE-New	0.35	0.40	0.48	0.55	0.58	0.28	0.09	0.10	0.12	47.56
RMSE-Ori	---	0.56	---	0.73	0.90	---	0.27	0.13	0.16	60.00

Perspectives

* Validation over a long period (1 year) and for others urban sites.



SURFEX coupled off-line to ALADIN: preliminary results over Belgium

ADAPTATION

DOWNSCALING

FULLPOS

ECOCLIMAP

ERA40

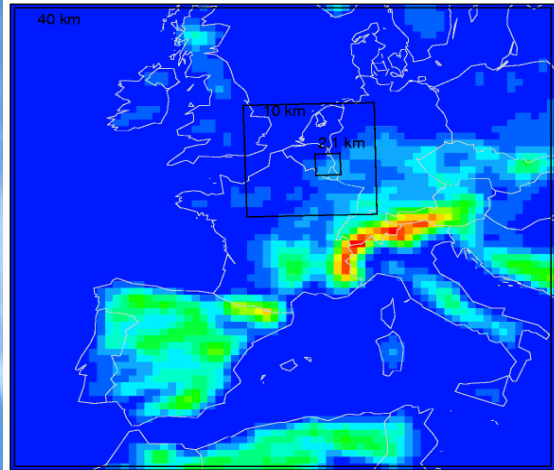
**10 km resolution
over Belgium**

**Atmospheric forcing at 50 m
T, P, Hu, Wind, Precipitation,
downward Radiation**

**SURFEX
(off-line)**

**T2m, H2m
wind10m**

ERA-40 downscaling domains

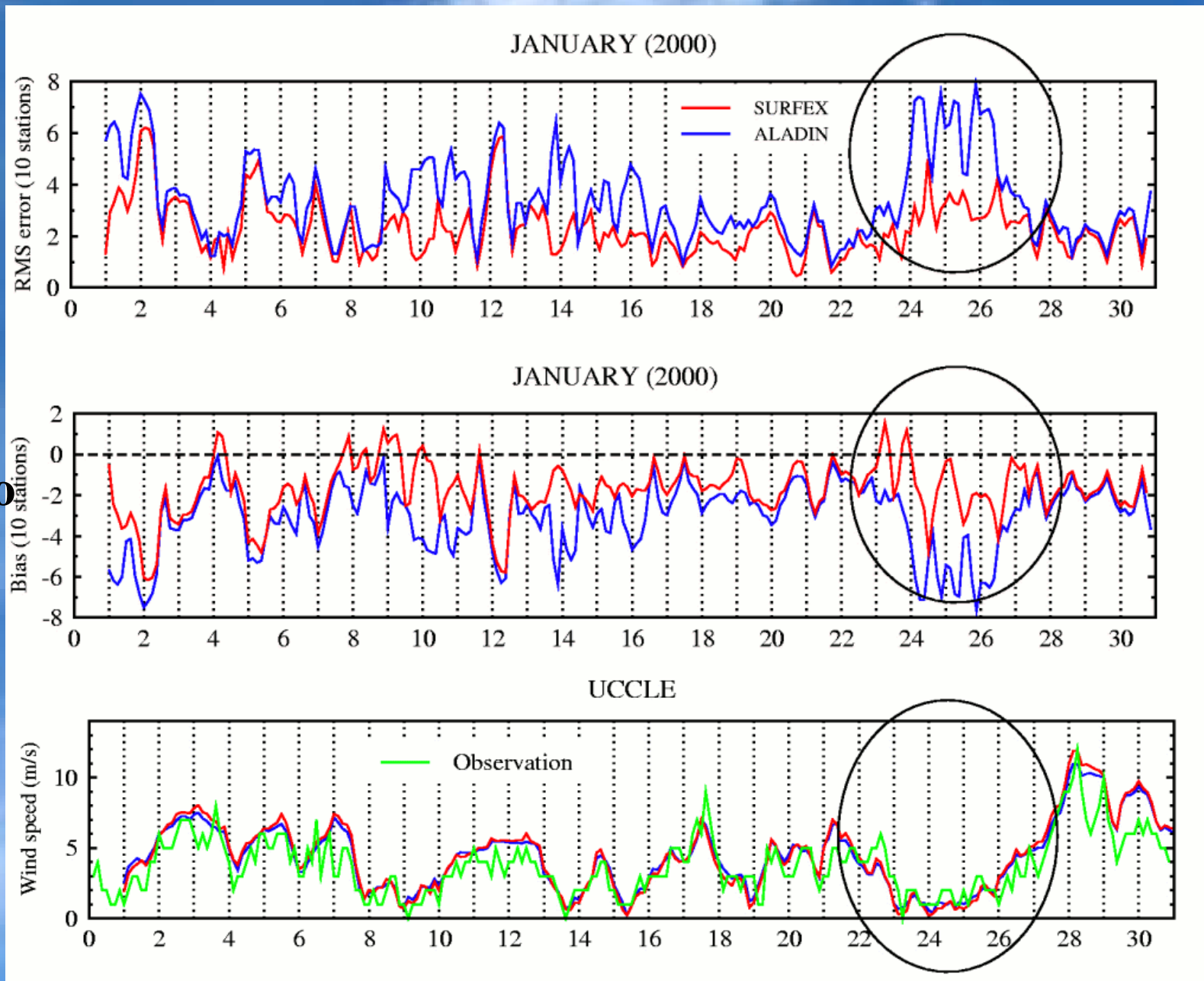


T2m

**SURFEX decreases
the RMS-error**

**ALADIN 2m T are too
low**

**Anticyclonic situation
with very weak wind**



The same result is found for winter 2001